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低電壓製程之電荷幫浦電路設計



Charge Pump Design in Low-Voltage CMOS Process Technology

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低電壓製程之電荷幫浦電路設計 Charge Pump Design in Low-voltage CMOS Technology

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低電壓製程之電荷幫浦電路設計

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摘要

電荷幫浦(charge pump circuits)能夠產生比輸入電壓(supply voltage)還要高的電位以及比基準電位(GND)還要低的電位。現今電荷幫浦主要用於非揮發性記憶體中 (nonvolatile memory),用來抹除資料或者是寫入資料,此外,為了能夠符合一般家用電規格,在LCD面板上同時也需要電荷幫浦來提高電壓以驅動面板的開關來達到色彩輸出。

因此,此篇論文提出一個新的電荷幫浦的架構,其目的是為了在沒有受到閘極可靠度(gate-oxide reliability)的影響之下,能夠減少漏電流(return-back leakage current)的產生,同時透過模擬以及實做來實現電路。透過量測可以驗證新的電路架構是否能正常工作以及是否有不錯的輸出效果。在1.8V的輸入電壓下,量測的輸出電位為8.8伏,此項結果可以驗證新的電路架構比傳統的電荷幫浦有較好的效能。同時也驗證在減少漏電流的情況以及沒有受到閘極可靠度的影響下,可以有效的提高輸出電壓。因此,新的電路架構是適合在現今的低電壓以及低功率的積體電路上。

Charge Pump Design in Low-voltage CMOS Technology

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ABSTRACT

Charge pump circuits are usually used to generate voltages higher than the available supply voltage. It is applied widely in EEPROM or flash memories to program the floating-gate device.

A new charge pump circuit has been proposed to suppress the return-back leakage current without suffering the gate oxide reliability issue in low-voltage CMOS process. A test chip has been implemented in a 65-nm CMOS process to verify the proposed charge pump circuit with four pumping stages. By inserting a short turn-off period into the circuit operation of charge pump circuit, the return-back leakage current during the clock transition can be successfully suppressed in the new proposed charge pump circuit. The measured output voltage is around 8.8V with 1.8V supply voltage, which is better than the conventional charge pump circuit with the same pumping stages. Because of reducing the return-back leakage current and without suffering gate oxide reliability issue, the new proposed charge pump circuit is suitable for the applications in low-voltage and low-power CMOS IC products.

This thesis is organized into six chapters and this introduction is the first one. Chapter 2

introduces design background for charge pump circuit used in memories. Chapter 3 introduces the prior arts of charge pump circuits, and the summary is summarized all the problems solved and not solved. In Chapter 4, a new charge pump circuit, without the gate oxide reliability issue, reducing the return-back leakage current is presented, and the simulated results is also shown in this chapter. Finally, the efficiency and the return charge are introduced at the last. In chapter 5, the layout view and the measured result is displayed. At the final chapter, Chapter 6, recapitulates the major consideration of this thesis and concludes with suggestions for future investigation.



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> 翁 怡 歆 謹 致 於 交大竹塹 已 丑 夏

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Chapter 1

Introduction

1.1 MOTIVATION

Charge pump circuits are usually designed to generate voltage higher than the power supply voltage (VDD) or lower than the ground voltage (GND) in a chip. They are frequently used to provide a voltage higher than a power supply because high voltage level in a charge pump is generated by transferring charges to a capacitive load without any amplifiers or regular transformers. Most modern charge pump circuits are designed according to Dickson charge pump circuit, and the MOS transistors are utilized to transfer the charges from stage to stage.

Charge pump circuits are suitable for applications in low-voltage CMOS integrated circuits. It can be applied to the nonvolatile memories, such as EEPROM or flash memories, to write or to erase the floating-gate devices. Moreover, charge pump circuits are also used in power management blocks, the driver ICs for liquid-crystal-display (LCD) panels, and USB OTG (on-the-go).

Some problems of conventional charge pump circuit, such as threshold drop, body effect, junction breakdown, and gate-oxide reliability issues had been studied. Nevertheless, it suffered the return-back leakage current during the clock transitions.

In this work, by reducing the return-back leakage current, the new proposed charge pump circuit is suitable for the applications in low-voltage and low-power CMOS IC products without suffering gate oxide reliability issue.

1.2 ORGANIZATION

This thesis is organized into six chapters and this introduction is the first one. Chapter 2 introduces design background for charge pump circuit used in memories. Chapter 3 introduces the prior arts of charge pump circuits, and the summary is summarized all the problems solved and not solved. In Chapter 4, a new charge pump circuit, without the gate oxide reliability issue, reducing the return-back leakage current is presented, and the simulated results is also shown in this chapter. Finally, the efficiency and the return charge are introduced at the last. In chapter 5, the layout view and the measured result is displayed. At the final chapter, Chapter 6, recapitulates the major consideration of this thesis and concludes with suggestions for future investigation.



Chapter 2

Background

2.1 Introduction of Charge Pump Circuits

The first charge pump circuit is called the Cockcroft-Walton voltage multiplier with the purpose of generating steady potential nearly 800,000 volts to power the particle accelerator, performing the first artificial nuclear disintegration. Fig. 2.1 shows the method of Cockcroft-Walton voltage multiplier [1]. K_1 , K_2 , K_3 , X_1 , and X_2 are the capacitors to storage charges. S_1 , S_1 , S_2 , S_2 , S_3 , and S_3 are utilized to transfer charges between the capacitors, and VDD is the supply voltage. When connecting the switches of S_1 , S_2 , and S_3 , it is expected that the voltage of n_1 is VDD. After that, connecting switches of S_1 , S_2 , and S_3 , the voltage of n_1 is 2VDD and the voltage of n_2 is 2VDD. In the next reversal of the switches, the voltage of n_3 is 2VDD. Finally, when it is connected with S_1 , S_2 , and S_3 , the voltage of n_4 , which is equal to n_3 is 3VDD. From this method, Fig. 2.2 shows the basic Cockcroft-Walton voltage multiplier composed of capacitors (C), where Cs is the parasitic capacitor, diodes, and clocks (CLK and CLKB) to form the voltage multiplier [2].

When CLKB is low and the CLK is high,

$$a = VDD - V_D. (2.1)$$

At the next half period, CLKB is high and the CLK is low,

$$a = VDD - V_D + VDD \times \frac{C}{x + C}$$
, and (2.2)

$$b = a - V_D. (2.3)$$

Next at another new period, CLKB is low and the CLK is high,

$$a = VDD - V_D, (2.4)$$

$$b = VDD \left(1 + \frac{C}{x + C} + \frac{C}{s + C}\right) - 2V_D$$
, and (2.5)

$$c = b - V_D. (2.6)$$

And the next, CLKB is high and the CLK is low,

$$a = VDD - V_D + VDD \times \frac{C}{x + C}, \qquad (2.7)$$

$$b = a - V_D, (2.8)$$

$$c = VDD \left(1 + \frac{C}{x + C} + \frac{C}{s + C} + \frac{C}{x + C} \frac{C}{y + C}\right) - 3V_D$$
, and (2.9)

$$d = c - V_D. (2.10)$$

Finally, CLKB is low and the CLK is high,

$$a = VDD - V_D, (2.11)$$

$$b = VDD \left(1 + \frac{C}{x + C} + \frac{C}{s + C} \right) - 2V_D, \qquad (1.12)$$

$$c = b - V_D, \qquad (1.13)$$

$$d = VDD \left(1 + \frac{C}{x+C} + \frac{C}{s+C} + \frac{C}{x+C} \frac{C}{y+C} + \frac{C}{s+C} \frac{C}{t+C} \right) - 4V_D, \text{ and}$$

$$e = d - V_D.$$
(1.14)

$$e = d - V_D. \tag{1.15}$$

Hence, the input impedance increases in each node with the number of multiplying stages, it means the output voltage is decreased as the number of stage is increased. Therefore, the Cockcroft-Walton voltage multiplier is inefficient, when integrated into the chip, due to its large stray capacitance and high output impedance.

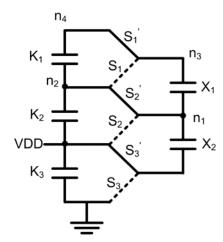


Fig. 2.1 The method of the Cockcroft-Walton voltage multiplier [1].

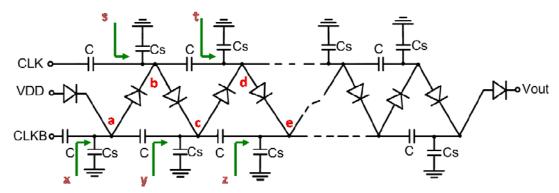


Fig. 2.2 It is Cockcroft-Walton voltage multiplier, and s, t, x, y, and z are the input impedances from their nodes [2].

2.2 APPLICATIONS OF CHARGE PUMP CIRCUITS

Charge pump circuits can generate the voltage higher than the power supply voltage (VDD) or lower than the ground voltage (GND) in a chip, usually used to write or erase data in nonvolatile memory[3]-[4]. Moreover, charge pump circuits are also used in power management blocks and the driver ICs for liquid-crystal-display (LCD) panels [5]. In mixed-mode circuit, it also needs to the charge pump circuit to generate higher voltage or negative voltage because there are more different supply voltage and VSS to be used.

Three main methods of programming and erasing data are Fowler-Nordheim tunneling (FN), band-to-band hot electron (BBHE), and channel hot-electron injection (CHEI).

In the program mode for NMOS, FN is that the gate terminal with the high voltage, where the source terminal is 0V and the drain terminal is floating, generate a high electron field to let the energy barrier of thin oxide like in Fig. 2.3, then the electron in the conduction band can tunnel through the triangular energy barrier to the floating gate shown in fig. 2.4. CHEI is that the device, where the gate terminal is the high voltage, the source terminal is 0V, and the drain terminal is a positive voltage smaller than the gate terminal, is turned on and then pinched up such that the hot-electron in the depletion region tunnel to the floating gate from the pinch up region. BBHE is that the drain terminal with the high voltage, where the gate terminal is

negative voltage and the source terminal is floating, let the energy band of the thin oxide be liked in Fig. 2.3 and make the electron tunneling to the floating gate.

In the erase mode for NMOS, there is only one way, FN, to erase. When the gate terminal is the negative voltage and the drain terminal is the small positive voltage, the electron in the floating gate will be rejected to tunnel to back the drain terminal. In another method, only the well of the cell with the high voltage let the electron in the floating gate tunnel to the well because of positive-negative electrode attracting.

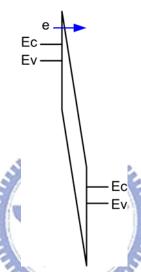


Fig. 2.3 The energy band of thin oxide in the flash memory cell.

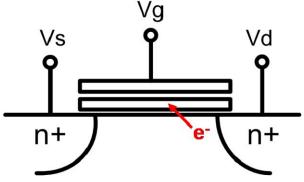


Fig. 2.4 The schematic of the flash memory cell.

Chapter 3

Prior Arts of Charge Pump Circuits

3.1 DICKSON CHARGE PUMP CIRCUIT

Since the Cockcroft-Walton voltage multiplier is inefficient, when it integrated into the chip due to its large stray capacitance and high input impedance. The Dickson charge pump circuit has been proposed to create a new voltage multiplier with higher efficiency, as shown in Fig. 3.1 [2], where CLK and CLKB are out of phase clocks, C is the pumping capacitor, Cs is the parasitic capacitor, Cout is the output capacitor loading, and R_L is the output loading. When the CLK is low (CLKB is high), the even-number diodes are turned off, and the odd-number diodes are turned on to transfer the charge from VDD to node a and node b to node c. Hence, the voltage of a, b, c, and d is

$$a = VDD - Vd, (3.1)$$

$$b = VDD \left(1 + \frac{2C}{C + C_s}\right) - 2Vd, \qquad (3.2)$$

$$c = b - Vd$$
, and (3.3)

$$d = VDD\left(1 + \frac{4C}{C + C_s}\right) - 4Vd, \qquad (3.4)$$

where Vd is the voltage drop of diodes.

When the CLKB is low (CLK is high), the odd-number diodes are turned off, and the even-number diodes are turned on to transfer the charge from node a to node b and node c to node d. Hence, the voltage of a, b, c, and d is

$$a = VDD - Vd + VDD \frac{C}{C + C_s}, \qquad (3.5)$$

$$b = a - Vd, (3.6)$$

$$c = VDD \left(1 + \frac{3C}{C + C_s} \right) - 3Vd, \text{ and}$$
 (3.7)

$$d = c - Vd. (3.8)$$

Finally, the output voltage is shown in (3.9),

$$Vout = VDD + N \left[\left(\frac{C}{C + C_s} VDD - Vd \right) \right] - Vd - \frac{NI_{out}}{(C + C_s)f},$$
 (3.9)

where the voltage drop in each stage due to the output current is

$$V' = \frac{NI_{out}}{(C + C_s)f}, \qquad (3.10)$$

where N is the stage number, Iout is the output current, and f is the clock frequency [6].

Fig. 3.2 is shown the Dickson charge pump circuit realized with NMOS, and the diode-connected NMOS is utilized to transfer charge from input to output in each stage [6]. When the CLK is low (CLKB is high), m1, m3, and m5 are turned on (m2 and m4 kept off), the charge is transferred from VDD to node1, the charge in node 2, which is pumping higher by CLK, is transferred to node 3, and the charge in node 4 pumping to higher voltage is transferred to Vout. On the other hand, when the CLK is high (CLKB is low), m2 and m4 are turned on (m1 and m3 kept off), the voltage of node 1 and node 3 become higher. At this moment, the charge is transferred from node 1 to node 2, and charge in node 3 is transferred to node 4. Therefore, the output voltage of Dickson charge pump circuit is

$$Vout = \sum_{i=1}^{N+1} \left(VDD \frac{C}{C + C_s} - V_{ti} \right), \tag{3.11}$$

where Vti denotes the threshold voltage of the diode-connected NMOS in the ith stage, and N is the stage number. If the Cs is too small to ignore, the output voltage becomes

$$Vout = \sum_{i=1}^{N+1} (VDD - V_{ti}).$$
 (3.12)

However, when each node is pumped higher, the threshold voltage in each NMOS becomes larger due to the body effect. Therefore, the efficiency of this circuit is decreased as the stage increases. Besides, it suffers overstress voltage across the gate oxide of devices when the voltages at each stage nodes are pumping higher. To avoid the gate-oxide overstress issue, the high-voltage device with thick gate oxide can be utilized for implementing such Dickson

charge pump circuit. However, the thick gate-oxide NMOS often has a high threshold voltage which somehow degrades the pumping efficiency.

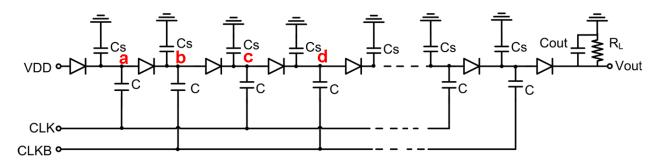


Fig. 3.1 Dickson charge pump circuit [2].

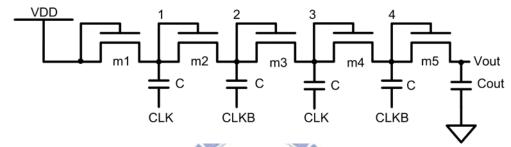


Fig. 3.2 Dickson charge pump circuit realized with NMOS [6].

3.2 CHARGE PUMP CIRCUIT WITH BOOSTRAPPED CIRCUIT

To restrain the body effect, Fig. 3.3(a) shows the charge pump circuit using boostrapped circuit [7], Fig. 3.3(b) shows its clock waveforms, and Table 3.1 shows the state of the clocks in different interval. This charge pump circuit is used PMOS to be the charge transfer device, as it has smaller leakage current than NMOS and its body and source can connect without extra masks.

The operations of this charge pump circuit are as following:

These four phases clock can be separated to six intervals, where the odd-number stages transfer charge at interval (1), (2), and (3), and even-number stages transfer charge at interval (4), (5), and (6).

At the interval (6) and (4)

When CLK1 is low and others are high, the device of M0 is turned on and others are

turned off. Hence, the voltage of the n1 node is VDD-Vt0, where Vt0 is the threshold voltage of M0, and the voltage of the n2 node is 4VDD-Vt0.

At the interval (1) and (3)

When CLK2 is low and others are high, M0 is turned off, the voltage of n1 is rose to 2VDD-Vt0, but n2 is dropped to 3VDD-Vt0, M4 is turned on to transfer charge from n3 to the gate of M3, and other devices are turned off. The voltage of n1 is 2VDD-Vt0.

At the interval (2)

When CLK1 and CLK4 are high, and CLK2 and CLK3 are low, M1 is turned on to transfer charge from node 1 to node2, and M2 is turned off. At the same time, the voltage of node 1 still kept 2VDD-Vt0, and the voltage of node 2 is the same with node 1.

At the interval (5)

When CLK1 and CLK4 are low, and CLK2 and CLK3 are high, M0 is still turned on, n1 is kept at VDD-Vt0, and n2 is also kept at 4VDD-Vt0. Moreover, M3 is turned on to transfer the voltage at n2 to n3, and others are kept off expect the transfer devices, M3, M5 and so on, at the even stage.

The boostrapped circuit is shown in Fig. 3.4. Using the boostrapped circuit can turn on the trsnsfer device certainly as the clocks connecting to the boostrapped circuit are at logic 0.

In the boostrapped circuit, when the input (Vin) is at logic 0, CLK is at logic 0, node 1 and node 6 are at logic 1, node 2 and node 3 are at logic 0, M3 is turned on to make node 7 be logic 0, Mp1 is turned on to let node 4 be at logic 1, and M1 will be turned on to transfer logic 0 from node 3 to node 5, where the capacitor storage charges since the difference voltages are at the two terminal of this capacitor. M2 is turned on to make node 5 be at logic 0 quickly, and then node 8 is at logic 1 to turn off Mp3. Therefor, the output voltage is at the mode of logic 0.

When the input is at logic 1, CLK is at logic 1, node 1 and node 6 are at logic 0, node 2 and node 3 are at logic 1, the M2 is turned off to cut off the current path from node 5, and Mp2 is turned on to keep the node 4 to hold at logic 1. Because node 3 becomes to logic 1, node 4

raises the voltage potential to the higher voltage and turn on M1 such that node 5 is with higher voltage potential. Therefore, Mp3 is turned on since node 8 is at logic 0; node 7 is at logic 1. Finally, the output voltage is with higher voltage than VDD.

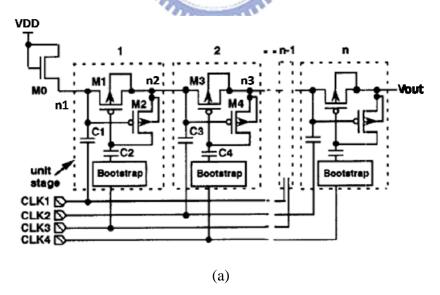
In the Dickson charge pump circuit, the voltage gain at i stage is given by

$$V_{gain,i} = \frac{C \bullet VDD}{(C + C_s)} - V_{ti}(V_{bs}), \qquad (3.13)$$

where $V_{ti}(V_{bs})$ is the threshold voltage with V_{bs} bias at the i stage. This equation indicates that the voltage gain is decreased and output voltage is not increased through using more stages due to the body effect. Although this prior art circuit can reduce the influence of the body effect, a threshold drop is still hold at NMOS and an extra circuit is used.

Table 3.1 The variation of the clock logic.

		40, 50, 50, 50, 50	MINISTER DE L			
Interval	(1)	(2)	(3)	(4)	(5)	(6)
CLK1	1.5/	1 :	13 1	0	0	0
CLK2	0	0	0	1	1	1
CLK3	1=\	0	1	1/5	1	1
CLK4	1	1	1	13	0	1



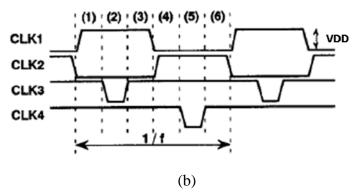


Fig. 3.3 (a) A charge pump circuit without body effect, and (b) its clock waveforms.

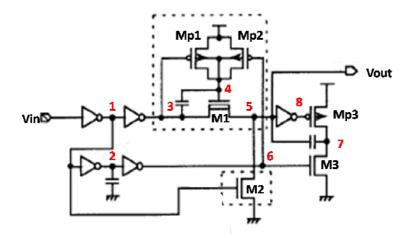


Fig. 3.4 The boostrapped circuit in the charge pump circuit.

3.3 FLOATING WELL CHARGE PUMP CIRCUIT (FWCP)

This charge pump circuits based on the Dickson charge pump circuit had been reported to enhance the pumping efficiency. Fig. 3.5(a) shows the floating-well charge pump circuit using the diode-connected PMOS as the charge transfer device [8]. The operation of this charge pump circuit is similar to the Dickson charge pump circuit, and the only difference is that the bulks of device in this charge pump circuit are floating. From the formula of the threshold voltage,

$$V_{t} = V_{t0} + \gamma \left[\sqrt{V_{bs} + 2\phi_{f}} - \sqrt{2\phi_{f}} \right],$$
 (3.14)

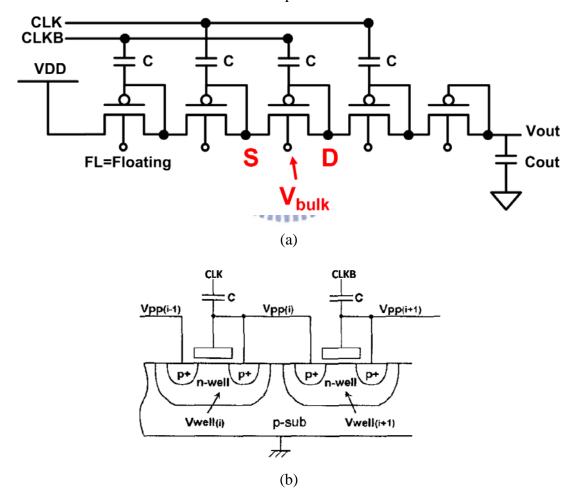
where V_{t0} is the threshold voltage without body effect, γ is the body effect coefficient, V_{bs} is the bias of the bulk and the source, and ϕ_f is the Fermi level. Since V_{bs} in all devices of the floating-well charge pump circuit are the same (V_{diode}), which cross section view is shows in

Fig. 3.5 (b), and the threshold voltage is

$$V_{te} = V_{t0} + \gamma \left[\sqrt{V_{diode} + 2\phi_f} - \sqrt{2\phi_f} \right], \tag{3.15}$$

where V_{diode} is the built-in potential of P+ to n-well diode. There are the parasitic diodes from the diffusion layer (P+) and n-well in PMOS, and these diodes are always turned on, so the voltage of the bulks (n-well) changes during the clock transition. The relative illustration is shown in Fig. 3.5 (c). If the D voltage is higher than the S voltage, the V_{bulk} is D voltage- V_{diode} . On the other hand, if the S voltage is higher than the D voltage, the V_{bulk} is S voltage- V_{diode} .

Although FWCP can reduce the influence of the body effect, it also induces the substrate current to disturb other circuits in the same chip.



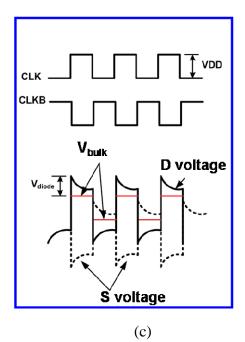


Fig. 3.5 (a) The floating-well charge pump circuit, (b) the cross section view of the one stage in this charge pump circuit, and (c) the variation waveform of clocks and the voltage potential of relative nodes.

3.4 CHARGE TRANSFER SWITCHES (CTS'S) CHARGE PUMP

Fig. 3.6 (a) shows a charge pump circuit that can be assigned to control the CTS's dynamically by using pass transistors MN's and MP's [9]. The CTS's in this circuit can be turned off completely when clock transfers and be turned on easily by the backward control.

First, when CLK is low (CLKB is high), MD1 is turned on to transfer VDD to node 1, and then the voltage of node 1 is VDD- V_{t1} , where V_t is the threshold voltage of MD1. And the same time, node 2 is pulled high to turn on MP1 (MD2is turned off), so MS1 is turn on to transfer charge to let the voltage of node 1 become VDD without the threshold drop. In this moment, MN2 is turned on to cut off MS2.

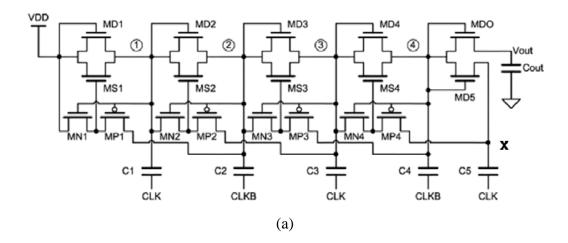
Second, when CLK is high (CLKB is low), the first stage is turned off and the second stage is turned on. Node 1 is pulled high to 2VDD, and MD2 is turned on to transfer charge from node 1 to node 2 (2VDD- V_{t2} , where V_{t2} is the threshold voltage of MD2). In addition, MP2 is turned on to open the switch (MS2), and the potential of node 2 will become 2VDD

completely. Besides, MN2 and MP1 are turned off, and MN1 is turned on to close the switch MS1 to avoid the current returning back to the forward node.

Following this operation step by step, it has high efficiency in this charge pump circuit, but there is a threshold drop at the last stage due to the body effect. To overcome this limitation, this circuit is added another circuit, in Fig. 3.6 (b), at the last stage to compensate the threshold drop.

In this clock generator, when CLK is low, the voltage of node b is VDD to turn on M1 and M3, then the voltage of node a is VDD and CLKB_h is VDD. At the next time, when CLK is high, the voltage of node b is 0 and node a is pulled high to 2VDD to turn on M2, then the potential of node b becomes VDD from low; hence, M3 is turned off and M4 is turned on to discharge CLKB_h to low. At the next period, CLK is low, the voltage of node a is back to VDD and the voltage of node b rise to 2VDD to turn on M3, and the potential of CLKB_h is 2VDD. And after this period, CLKB_h oscillates at 0 to 2VDD with 2VDD amplitude.

This charge pump circuit utilizes switches to transfer charge without the threshold drop, but it will has the threshold drop at the last stage without using the clock generator. However, it is a consideration where the bulk of M3 is connected, if using the clock generator in this charge pump circuit.



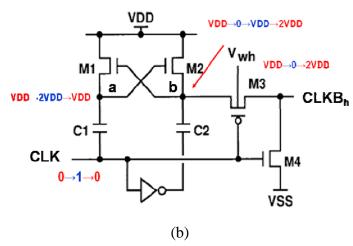


Fig. 3.6 (a) The CTS's charge pump circuit, and (b) a high-voltage clock generator.

3.5 CHARGE PUMP CIRCUITS WITH AUXILIARY CIRCUITS

3.5.1 The Charge Pump Circuit with an Auxiliary Circuit

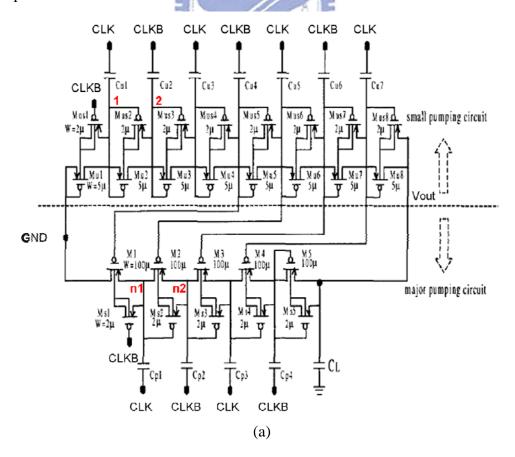
This charge pump circuit used small pump circuit to control the gate terminal of devices in the major pump circuit and used switches to control the bulk of the major device to avoid the body effect [10]. Fig. 3.7 (a) shows the negative pump circuit to generate the negative voltage, and Fig. 3.7 (b) shows the high positive pump circuit to generate the positive voltage. For the small pump circuit

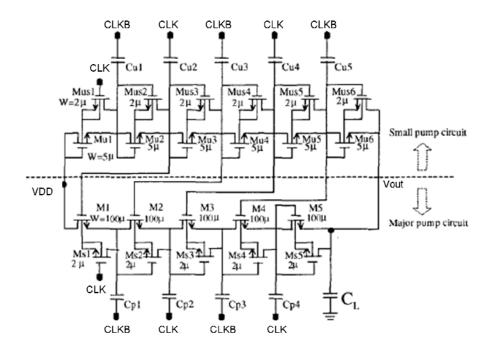
When CLKB=0 (CLK=1), Mu1 is turned on to let the potential of node 1 be GND+ |Vtp| and without the body effect, because Mus1 is turned on to connect bulk of Mu1 and node 1. When CLKB=1 (CLK=0), all the devices in the first stage are turned off, the voltage of node 1 is –VDD, and Mu2 and Mus2 are turned on to work the same function like the first stage. For the major pump circuit

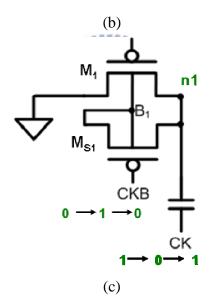
In the ideal situation, when CLKB=0 (CLK=1), the M1 is turned on to make the potential of node n1 be GND+ |Vtp| due to the gate terminal of M1 is connected to negative voltage. At the same time, Ms1 is turned on to connect the bulk of M1 and node n1. However, in Fig. 3.7 (c), when CLK=1 (CLKB=0), M₁ is turned on to let the potential of n1 be GND+ |Vtp|, and the potential of B₁ is also GND+ |Vtp| because of M_{s1} turned on. When CLK=0 (CLKB=1), the

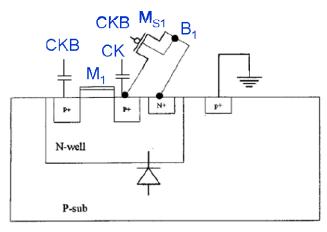
voltage of node n1 is dropped to -VDD+|Vtp| instantly through clock transition, and then M_1 still kept on charging node n1 to GND due to the negative bias at the gate terminal of M_1 , where M_{s1} are turned off. At the next period (CLK=1 and CLKB=0), node n1 does not become GND yet, M1 and Ms1 are turned on again, and the voltage of n1 is charged to the positive voltage higher than GND because B_1 (GND+|Vtp|) charges n1 to increase the potential of n1 and decrease its potential by itself. Hence, at the steady state, the potential of B1 and n1 will become to GND. In addition, it is due to the small pump circuit that the voltage gain is still held at the certain value. The relative simulation is shown in Fig. 3.8. Therefore, the pumping speed of this charge pump circuit is slow due to the small size devices of the small pumping circuit.

Another disadvantage of this negative circuit is the substrate leakage current. When the bulk of device becomes negative potential, the parasitic diode (p-sub to n-well) will turn on to charge the bulk to GND. Consequently, the negative major pump circuit is difficult to keep the negative potential.









(d)

Fig. 3.7 (a) The positive and (b) the negative charge pump circuits with an auxiliary circuit. (c) The steps of the first stage and (d) its cross section view.

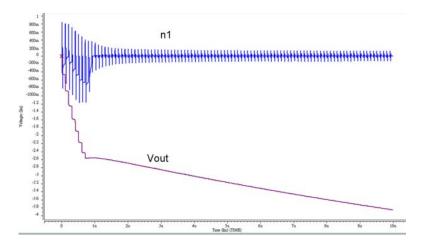


Fig. 3.8 The waveforms of n1 node and the output voltage on the negative pump circuit. The supply voltage is 1.8V, pumping capacitor is 10pF, loading capacitor is 20pF, and the other devices are the same with this paper [10].

3.5.2 Charge Pump Circuit Using Auxiliary Circuits

Fig. 3.9 shows the charge pump circuit by using two small circuits, a new small pump circuit and body bias circuit [11], and its performance is better than the prior art [10]. The new small circuit is used to control the potential of the gate terminal of the charge transfer devices in the major circuit, and the body bias circuit is used to reduce the leakage generated by the parasitic P-N junction.

When the CLK is high and CLKB is low, Ms1 and Ms2 are turned on to transfer charge from node 1, GND+ |Vtp| to GND, and M1 is turned on to let node n1 to GND in the major circuit since the gate terminal is connected to negative potential. At the same time, Mb1 is turned on to transfer charge from node b1, GND+ |Vtp|, to GND to control the body bias of the device in the major circuit.

When the CLK is low and CLKB is high, node 1 becomes –VDD+ |Vtp|, n1 is –VDD, and b1 is drop to –VDD+ |Vtp|. All the devices in the first stage of three circuits are turned off, and all the devices in the second stages are turned on to transfer charge from the next nodes to the

forward nodes. During the clock transition, two capacitors in the third stage have to charge Cs2, so the speed of voltage drop will slow down. This influence will slow down the speed of voltage drop of the gate bias, and reduce the reverse current.

This circuit could solve the problem the forward charge pump generating, but it has the body effect issue in three circuits. In addition, it is used more circuits and devices to occupy more area of charge pump circuit.

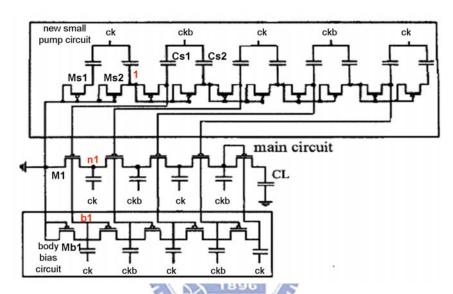


Fig. 3.9 The charge pump circuit with two small circuits.

3.6 CHARGE PUMP CIRCUIT USING AUXILIARY MOSFET

By using auxiliary MOSFET to eliminate the body effect, shown in Fig. 3.10, this charge pump circuit has not bad efficiency [12]. When CLK is low and CLKB is high, M1 is turned on to transfer charge from VDD to node 1, and then the voltage of node 1 is VDD-|Vtp|. In the meanwhile, Ma2 is turned on to connect the charge transfer device (M1) to node 1 so that this device is not the body effect issue. At the next half period, CLK is high and CLKB is low, M1 and Ma2 are turned off, Ma1 is turned on to connected the bulk of M1 to VDD, and the charge transfer devices in the second stage is turned on to transfer charge from node 1 to node 2. Hence, the output voltage is

$$V_{out} = N \times (VDD - |V_{tD}|) + VDD.$$
 (3.16)

The bulk of charge transfer devices are always connected to the higher voltage through controlling the turn on time of auxiliary MOSFET dynamically. However, it increases the parasitic capacitance due to use extra MOSFET connected to the pumping capacitors.

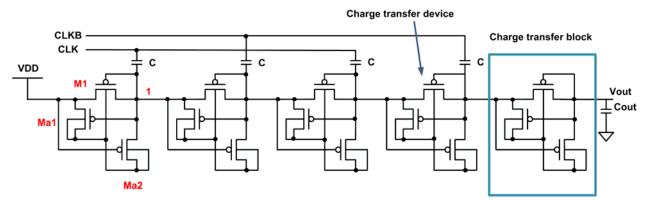


Fig. 3.10 The charge pump circuit by using auxiliary MOSFET.

3.7 New Four-Phase Charge Pump Circuit

This circuit is based on the Dickson charge pump circuit with four-phase clock to achieve its function more effectively [13]. Fig. 3.11 (a) shows the four-phase charge pump circuit, Fig. 3.11 (b) shows the clock waveforms, and Table 3.2 shows the states of the clocks in different interval.

At the T_1 and T_7

CLK1, CLK2, CLK3, and CLK4 are 0, 0, 1, and 0, so Ms1 is turned on to transfer charge from VDD to node s1, where the voltage of s1 is VDD. At this moment, node 1 are rose to 2VDD from VDD.

At the T_2 and T_6

CLK1, CLK2, CLK3, and CLK4 are 1, 0, 1, and 0, so Ms1 is still turned on and Ms2 are turned on to transfer charge from node 1 to s2, where node s2 becomes 2VDD. Node 1 and s1 are still hold on VDD and 2VDD.

At the T₃ and T₅

CLK1, CLK2, CLK3, and CLK4 are 1, 0, 0, and 0, so all the devices in first stage and second stage are hold at the forward condition except Ms1, which is turned off.

At the T_4

CLK1, CLK2, CLK3, and CLK4 are 1, 1, 0, and 0, so M1 is turned on to transfer charge from VDD to node 1 because node s1 is rose to 3VDD due to the double amplitude of CLK2. At the T_8

CLK1, CLK2, CLK3, and CLK4 are 0, 0, 1, and 1, so Ms1 is turned on and s1 is fell down to VDD to turn off M1. At the same time, s2 becomes 4VDD to turn on M2 to transfer charge from node 1 to node 2.

From these steps, the charge from input can transfer to the output, but this circuit needs more other circuits to generate the four-phase clock, shown in Fig. 3.12 (a), the delay circuit (b), and the double amplitude (c).

The disadvantage of this charge pump circuit is more additional circuits are utilized for charge pump circuit used and also have large layout area.

Table 3.2 The states of clocks in the different intervals.

	T_1	T_2	T_3	T_4	T_5	T_6	T_7	T_8
CLK1	0	1	1	1	1	1	0	0
CLK2	0	0	0	1	0	0	0	0
CLK3	1	1	0	0	0	1	1	1
CLK4	0	0	0	0	0	0	0	1

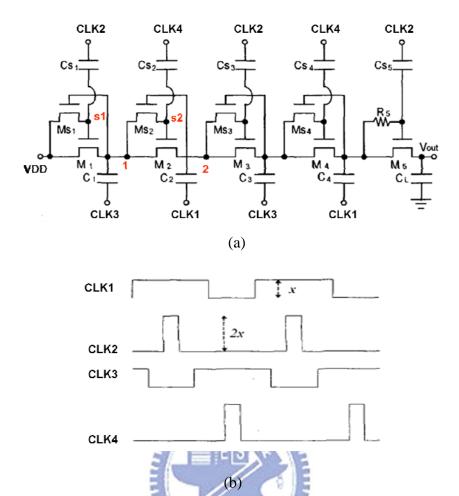
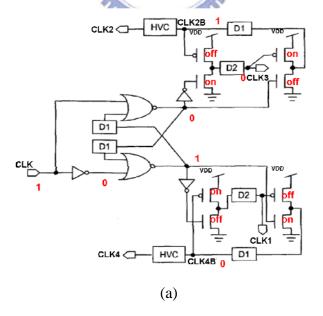
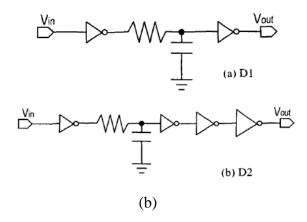


Fig. 3.11 (a) The four-phase charge pump circuit, and (b) the clock waveforms.





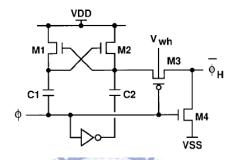


Fig. 3.12 (a) The four-phase clock generator, (b) the delay circuit, and (c) high-voltage circuit (HVC).

3.8 CHARGE PUMP CIRCUIT USING ALL PMOS DEVICES

In [14]-[15], they utilized the PMOS with lower sensitivity of threshold voltage to temperature and body bias to implement the charge pump circuit without gate oxide reliability issue in a low-voltage CMOS process. However, it also increased parasitic capacitance and degraded the speed of charge pump circuit due to more devices connected to the pumping nodes.

3.8.1 Charge Pump Circuit with Four-Phase Clock

Because the source and bulk can be connected in PMOS without any extra masking, it is used all PMOS device in this charge pump circuit [14], in Fig. 3.13 (a) and (b).

At the first interval, P1 is turned on to transfer charge from Vin to Vout and then turned

off. Simultaneously, P3 is turned off and then turned on to transfer charge from node 1 to node 4. Hence, the voltage of node 1 is a little higher than Vin and node 4 is Vin+|Vtp|. From the upper part, P5 is turned on to transfer Vin+ VDD in the node 2 to Vout, and P6 is turned on to let node 3 become Vin+VDD*, where

$$VDD^* = VDD \times \left(\frac{C_{aux}}{C_{aux} + C_{paraux}}\right).$$
 (3.17)

At the second interval, P3 and P6 are turned on to transfer charge from node 1 and node 2 to node 3 and node 4, the voltage of node 1 and node 2 are Vin+ VDD, and the potential of node 3 and node 4 are Vin+VDD*.

At the third interval, P3 and P6 are still turned on and P2 is turned on to transfer Vin+VDD from node 1 to Vout. At the same time, the voltage of node 2 is a little higher than Vin and the potential of node 3 becomes Vin+ |Vtp|.

The fourth interval to the sixth interval is similar to the first interval to the third interval, but the turn-on devices in these intervals are symmetrical to the time of the first interval to the third interval to transfer charge from Vin to Vout.

However, this charge pump circuit is its limitation. For example, if P4 is turned on, the voltage difference of source to gate has to becomes

$$VDD - \left(Vin + |Vtp| - VDD \times \frac{1}{1 + \frac{C_{paraux}}{C_{aux}}} \right) > |Vtp|.$$
 (3.18)

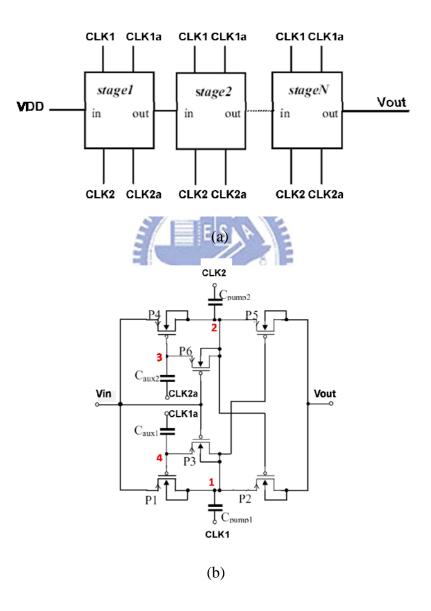
On the other hand,

$$V_{ov} = VDD - 2 | Vtp | - \frac{I_{out}}{fC_{pump}}, \qquad (3.19)$$

where Vtp is the threshold voltage of PMOS, C_{paraux} is the parasitic capacitor at the C_{aux} side, C_{aux} is the auxiliary capacitor, Iout is the output current, f is the clock frequency, and C_{pump} is the pumping capacitor. Therefore, it has the limitation for the lowest supply voltage, so it is unsuitable for low-voltage process.

Table 3.3 The clock logic table of the charge pump circuit using PMOS devices.

CLK1a	0->1	1	1	1	1	1
CLK1	0	1	1	1	1	0
CLK2	1	1	0	0	1	1
CLK2a	1	1	1	0->1	1	1



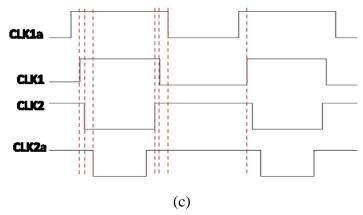


Fig. 3.13 (a) The block diagram of the charge pump circuit using all PMOS devices, (b) The one stage of this charge pump circuit, and (c) its clock waveforms.

3.8.2 The Six-Phase Charge Pump Circuit

Fig. 3.14 shows the charge pump circuit utilized six-phase clock with four-stage [15]. In Fig. 3.14 (b), it is utilized a voltage level shift in this circuit and has two branched to transfer charge from input to Vout alternately.

At the T1 interval, Ma3 is turn on to let node dr3 become Vin+VDD, Mp3 is turned on to transfer charge to Vout, and other devices are turned off. At this time, the voltage of dr1, dr2, and Net2 are Vin, and dr4 is from Vin to Vin-VDD and then to Vin when CLKE changes from VDD to 0 and the to VDD.

At the T2 interval, Ma3 is still turned on to connect Net 1 and dr3 with the voltage, Vin, and the voltage shift is worked to change the voltage of Ca1 to Vin-VDD as Ma2 is turned on.

At the T3 and T4 intervals, the operation is liked to at the T1 and T2 intervals but the difference is the another branch to work, such as Ma4, Mp4, Mp1at T3 interval, and Ma1and Ma4 at T4 interval.

By using this charge pump circuit, it could operate at low-voltage process, because of
$$Vin-(Vin-VDD)>|Vtp|\Rightarrow VDD>|Vtp|\,, \eqno(3.20)$$

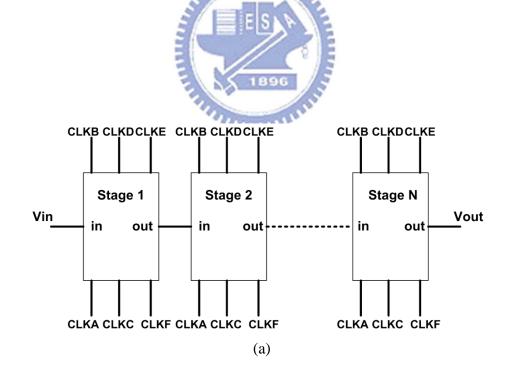
when Ma3 is turned on.

Although these charge pump circuit with all PMOS devices could have better efficiency, but it used much more devices and multi-phase clock to control these circuit. Hence, it can

consume extra power at other circuits. In addition, there are larger parasitic capacitors in PMOS than NMOS, and the pumping speed of PMOS charge pump circuits is slower than NMOS.

Table 3.3 The clock logic table for six-phase clock.

Thomas	Intervals				
Items	T1 Interval	T2 Interval	T3 Interval	T4 Interval	
CLKA	VDD	0	0	0	
CLKB	0	0	VDD	0	
CLKC	VDD	0	VDD	VDD	
CLKD	VDD	VDD	VDD	0	
CLKE	VDD->0->VDD	VDD	VDD	VDD	
CLKF	VDD	VDD	VDD>0->VDD	VDD	



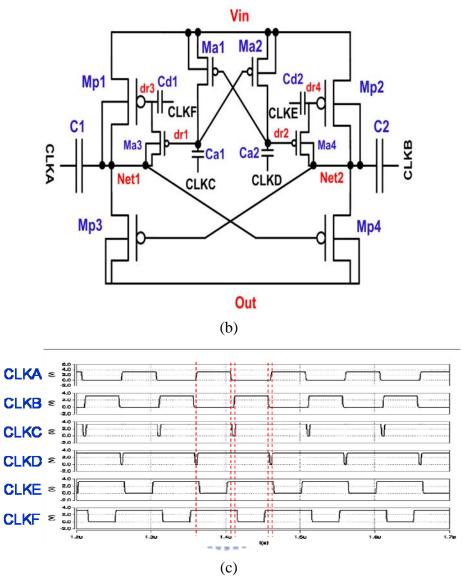


Fig. 3.14 (a) The six-phase charge pump circuit with four-stage, (b) the one stage circuit of this charge pump circuit, and (c) its clock waveforms.

3.9 THE CHARGE PUMP CIRCUIT WITHOUT GATE OXIDE RELIABILITY ISSUE

Due to the fact that the CMOS technology is continuously scaled down, some modified charge pump circuits based on Dickson charge pump circuit were invented to eliminate the body effect, to overcome the threshold drop, and to improve the efficiency. However, those charge pump circuits are suffered by the gate oxide reliability issue.

Fig. 3.15 shows the charge pump circuit designed with low-voltage devices but without suffering the gate oxide reliability issue because of no overstress voltage across it during the

circuit operation [16]. CLK and CLKB are out-of-phase with the amplitude of VDD.

When CLK is low (CLKB is high), mn5 is turned on to transfer charge from VDD to node 5, and mp1 is turned on to transfer charge from node 1 to node 2, the output of the first stage. Furthermore, the voltage of node 1 and node 2 are 2VDD, and node 5 is VDD. At the next half period, CLK is high and CLKB is low, mn1 is turned on to connect input (VDD) and node 1 became to VDD due to the low logic of CLKB, and mp5 is turned on to connect node 5 and output of the first stage, the same with node 2. In the meanwhile, the voltage of node 1 is VDD, node 5 is 2VDD, and the node between of mp5 and mn6 is 2VDD.

This circuit used two branches to avoid the gate oxide reliability, where the voltage difference between the drain/source and the gate in each MOSFET is not over VDD. This circuit has no threshold drop through using switches to transfer charge from input to output. However, in this charge pump circuit, the return-back leakage current during the transition of clocks will cause some degradation on the output voltage (Vout). For example, shown in Fig. 3.16, when CLK from high to low (CLKB from low to high), the voltage of node 1 becomes VDD from 2VDD, the voltage of node 5 becomes 2VDD from VDD, and the voltage of node 2 still holds in 2VDD. Hence, it is expected that mn1 in Fig. 3.15 has to be turned off and simultaneously mp1 in Fig. 3.15 has to be turned on. Actually, mn1 could not be turned off immediately but mp1 was turned on already, so mn1 and mp1 would provide a leakage path such that the voltage at node 2 will return back from 2VDD to VDD through mp1 and mn1 to the input node of VDD.

From the simulation of the leakage current in this charge pump circuit, in Fig. 3.17, the leakage current of PMOS is positive current and of NMOS is negative current. Moreover, it is the largest quantity of the leakage current in the last stage, and for this circuit, there are about 100µA to consume the power.

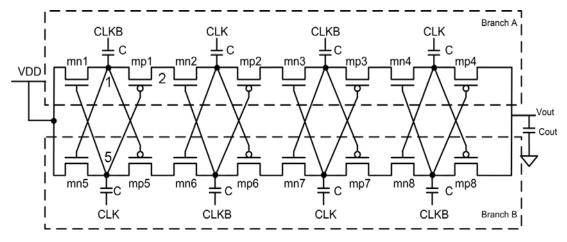


Fig. 3.15 The charge pump pump circuit with no gate oxide reliability issue.

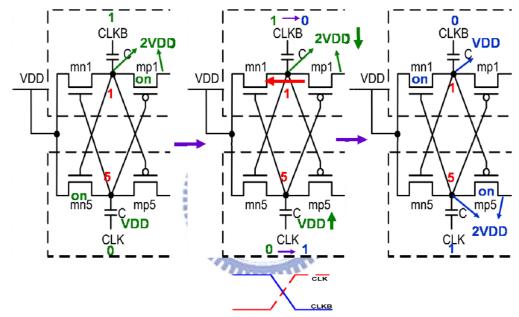


Fig. 3.16 The leakage path during the clock transitions.

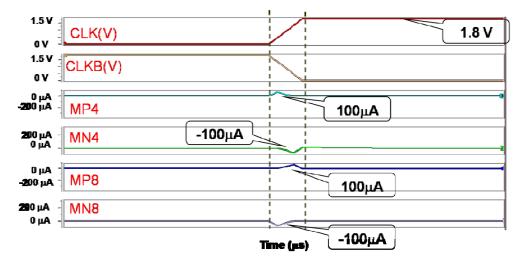


Fig. 3.17 The simulation waveforms of the leakage currents.

3.10 SUMMARY

Because the CMOS technology is continuously scaled down, the overstress limitation of the gate oxide has to be overcome. For the supply voltage becomes more and more lower, it has more and more opportunities to use charge pump circuit to generate higher voltage than VDD or lower voltage than GND. Nevertheless, there are more problems produced as the charge pump circuit used due to the process scaling down. From the prior arts, many circuits are used to solve some problems like the body effect, threshold drop, overstress on the gate oxide, and poor efficiency. However, it is serious for the advanced processes that there is a leakage current path in these charge circuits.



Chapter 4

The New Proposed Charge Pump Circuit

4.1 Introduction

For preventing the return-back leakage current, it has the time interval between the clock transitions to alternate the turn-on time of devices. Moreover, it needs more clock signals to control the extra time interval, and the time has to be shorter to avoid the degradation of Vout. Therefore, it needs additional devices and clocks to control the turn-on time of the charge transfer devices in the new proposed charge pump circuit.

4.2 THE OPERATION OF THE NEW PROPOSED CHARGE PUMP CIRCUIT

The new charge pump circuit is proposed to suppress the return-back leakage current in the prior-art circuit during clock transitions, and therefore its pumping efficiency can be further improved for implementation in the low-voltage CMOS processes.

Fig. 4.1 (a) shows the new proposed charge pump circuit with the corresponding clock waveforms shown in Fig. 4.1 (b). The all clock signals (CLKA, CLKB, CLKC, and CLKD) are non-overlapping with the amplitude of VDD. C is the main pumping capacitor, and Cs is the auxiliary pumping capacitor with a small capacitance. With PMOS (mc1, mc2, mc3, mc4, md1, md2, md3, and md4) of small device dimension and the auxiliary Cs capacitors to control the main charge transfer devices (mp1, mp2, mp3, mp4, mp5, mp6, mp7, and mp8) turning off properly, the return-back leakage current during the clock transitions can be avoided. Branch A and Branch B are identical but their turned-on periods are separated in the time domain. Branch A and Branch B are alternately operated to pump output voltage to high.

During the Interval T_1

During the interval T_1, CLKA, CLKB, CLKC, and CLKD are high, low, high, and high to low, respectively. At this moment, the voltage difference V15 (V37) between node 1 and node 5 (node 3 and node 7) is –VDD; hence, mn1 and mc1 (mn3 and mc3) are turned on to transfer charge from input node of VDD to node 1 (node 2 to node 3) and transfer charge from node 5 (node 7) to node c1 (c3). At the same moment, mp5 and mn6 (mp7 and mn8) are turned on to transfer charge from node 5 to node 6 (node 7 to node 8). Simultaneously, mn5 (mn7) is kept off to cut off the leakage path from node 5 back to input node of VDD (node 7 back to node 6), and mp1 and mn2 (mp3 and mn4) are kept off to cut off the leakage path from node 2 back to node 1 (node 4 back to node 3).

Hence, for the output stage, mp4 and mn8 are turned on (mn4 and mp8 are kept off,), and the pumping voltage will be transferred from node 4 to the output.

During the Interval T_2 and T_4

During the interval T_2 and T_4, CLKA, CLKB, CLKC, and CLKD are low, low, high, and high, respectively. At this period, the main charge transfer devices (mn1, mn2, mn3, mn4, mn5, mn6, mn7, and mn8) are turned off because all the voltage difference from gate to source of charge transfer devices are zero. In the meantime, the PMOS (mc1, mc2, mc3, mc4, md1, md2, md3, and md4) of small device sizes are turned on to rise the node c1/d1, c2/d2, c3/d3, and c4/d4 to the voltage level of 2VDD, 3VDD, 4VDD, and 5VDD, respectively. Therefore, the gate voltages of all charge transfer PMOS devices (mp1, mp2, mp3, mp4, mp5, mp6, mp7, and mp8) are higher than their corresponding source voltages to keep themselves off.

During the Interval T_3

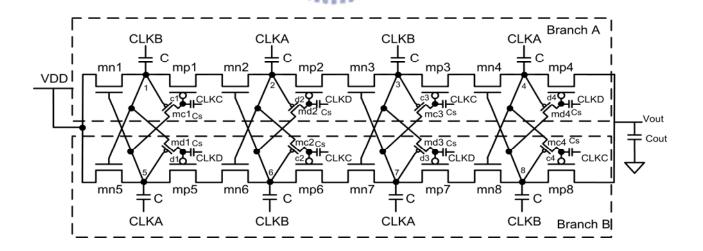
During the interval T_3, CLKA, CLKB, CLKC, and CLKD are low, high, high to low, and high, respectively. At this moment, the voltage difference V15 (V37) between node 1 and node 5 (node 3 and node 7) is VDD; hence, mn5 and md1 (mn7 and md3) are turned on to transfer charge from the input node of VDD (node 6) to node 5 (node 7), and transfer charge

from node 1 (node 3) to node d1 (d3). At the same moment, mp1 and mn2 (mp3 and mn4) are turned on to transfer charge from node 1 to node 2 (node 3 to node 4). Simultaneously, mn1 (mn3) is kept off to cut off the leakage path from node 1 back to the input node of VDD (node 3 back to node 2), and mp5 and mn6 (mp7 and mn8) are kept off to cut off the leakage path from node 6 back to node 5 (node 8 back to node 7).

Hence, for the output stage, mp8 and mn4 are turned on (mn8 and mp4 are kept off), and the pumping voltage will be transferred from node 8 to the output.

Table 4.1 The clock logic table. There are four periods of circuit operation in this new design.

	T_1	T_2	T_3	T_4
CLKA	1	0	0	0
CLKB	0,111	0	1	0
CLKC	1	ES	1->0	1
CLKD	1->0	1896	WHI.	1



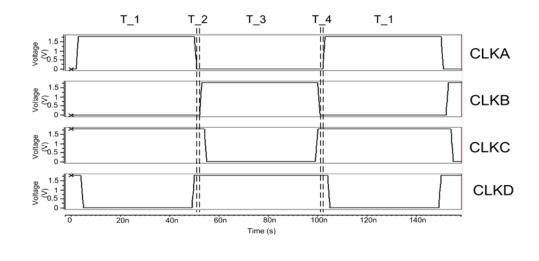


Fig. 4.1 (a) New proposed charge pump circuit, and (b) the corresponding clock waveforms.

(b)

4.3 SIMULATED RESULTS

A 65-nm CMOS process model with 2.5-V devices is used to simulate and the new proposed charge pump circuit, the prior-art circuit, and Dickson charge pump circuit. To have a fair comparison, the new proposed charge pump circuit and the prior-art circuit of Fig. 3.15 are designed with the same pumping capacitors (C) of 2pF, 4pF for Dickson charge pump circuit, the power supply VDD of 1.8V, the clock frequency of 10MHz, the same size dimensions of charge transfer devices, and the same output loading capacitor of 20pF. Additionally, the auxiliary capacitor (Cs) in the new proposed charge pump circuit is designed with 25fF. Ideally, the output voltage of four-stage charge pump circuit with power supply voltage 1.8V is 9V.

4.3.1 Simulations and Comparisons with the Prior Art [16]

Fig. 4.2 shows the simulated voltage waveform of each node in the new proposed charge pump circuit with four-stage to verify the gate oxide reliability issue, and the output voltage of this work is 8.85V with the supply voltage is 1.8V. Fig. 4.3 shows the leakage current waveforms to compare the result in Fig. 3.17. The simulated output voltage of the new proposed charge pump circuit is 8.85V in Fig. 4.4, the output voltage of prior-art circuit (Fig.

3.15) is only 8.28V, and the output voltage of Dickson charge pump circuit is 5.46V, where the rise/fall time of all clock signals is 1ns. In addition, when the rise/fall time of clock signals is increased, the time period of the return-back leakage current will become longer, so the quantity of return-back leakage current will increase during the clock transitions.

To estimate the return-back leakage current, Fig. 4.5 shows the method how to calculate it. For the PMOS, the return-back leakage current is positive. It can be approximately calculated, with its peak value and the time period that the leakage happened, by using the formula of triangle area. Finally, the estimated return charge is the result of adding all leakage currents (all the triangles) during the same period of clock transition. Similarly, for the NMOS, the return-back leakage current is negative, and the estimated method is the same as that with PMOS. The estimation result of return charge is shown in Fig. 4.6 under the clock signals with different rise/fall time. From this simulated/estimated results, the new proposed charge pump circuit has much smaller leakage current than that in the prior-art circuit of Fig. 3.15. In Fig. 4.7, when the rise/fall time of clock signals is increased, the time period of return current happened is also increased, and therefore the output voltage of the prior-art circuit is significantly decreased. However, by using this new proposed design, the degradation on the output voltage of charge pump circuit due to the long rise/fall time in the clock transition can be rescued.

Vout	8.85V	
Node 4	8.85V	7.09V
Node 8	7.09V	8.85V
Node 3	5.33V	7.09V
Node 7	7.09V	5.33V
Node 2	5.33V	3.57V
Node 6	3.57V	5.33V
Node 1	1.8V	3.57V
Node 5	3.57V	1.8V
26.46u 26.48u	26.5u 26.52u 26.54u Time (s)	26.56u 26

Fig. 4.2 The simulated voltage waveforms at the nodes 1~8 and the output (Vout) in the new proposed charge pump circuit with VDD of 1.8V.

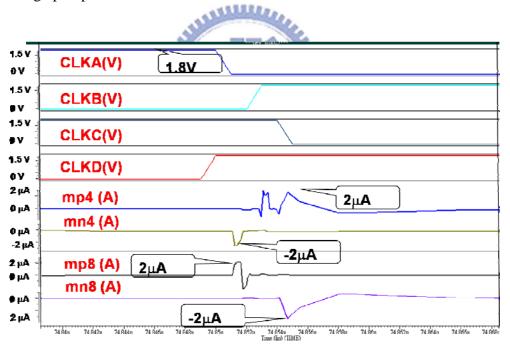


Fig. 4.3 The leakage currents of the new proposed charge pump circuit.

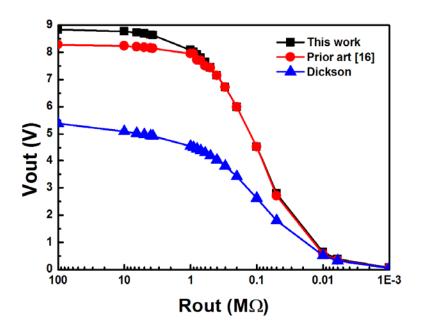


Fig. 4.4 The variations of the output voltages with different output loading.

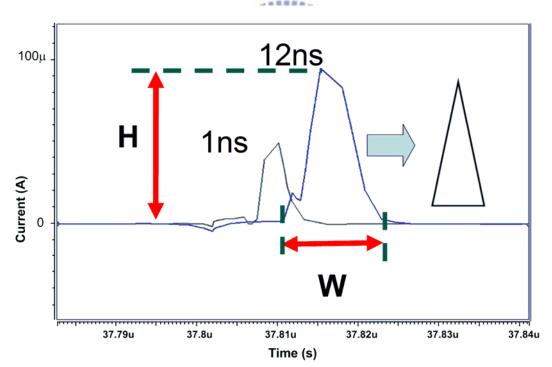


Fig. 4.5 The method used to estimate the return charge during the clock transition in the charge pump circuit. In this figure, two cases with rise/fall time of 1ns and 12 ns are demonstrated to approximately calculate the return charge with the formula of triangle area.

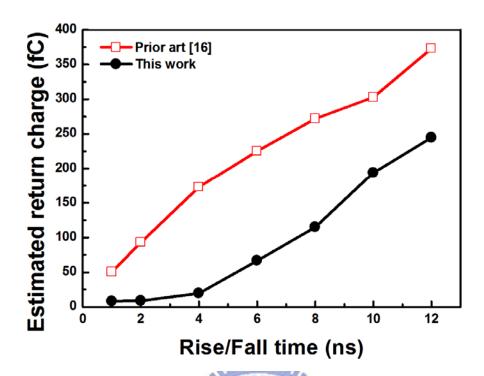


Fig. 4.6 The estimated return charge of the charge pump circuits under with different rise/fall time in the clock signals (f=10MHz, VDD=1.8V).

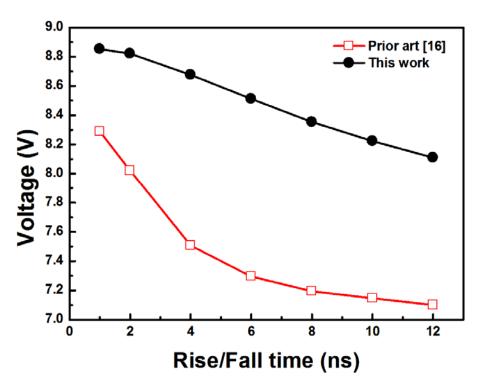


Fig. 4.7 The simulated output voltage of the charge pump circuits under with different rise/fall time in the clock signals (f=10MHz, VDD=1.8V).

4.3.2 Simulation of the Efficiency

Efficiency is a main point to test how better the charge pump circuit is, and the power consumption is relative with the efficiency [17]. The calculate the efficiency rule is

Efficiency(%) =
$$\frac{I_L \bullet V_{out}}{I_{power} \bullet V_{DD}}$$
, (4.1)

where

$$I_{power} = (N+1) \bullet I_{L} + I_{s}$$

$$(4.2)$$

and

$$I_{s} = N \bullet C_{p} \bullet f \bullet V_{DD}. \tag{4.3}$$

From Fig. 4.8 (a) and (b), they show why the reason of the input current is N+1 times of the output current. At the transient time, the charges from input are transfer to the output in every period and become more from the clock providing, so the charges will be transferred from stage by stage and enhanced by clock signals. When it is operated at the steady state, the output stage is exported 5Q in every period for the example in Fig. 4.8 (a). Fig. 4.8 (b) shows the voltage waveform of some pumping node of a charge pump circuit, the voltage drop is the result of that the leakage current flows to the parasitic capacitors after this node is pumped highly. Therefore, the total input current is (a) + (b) when a charge pump circuit is working.

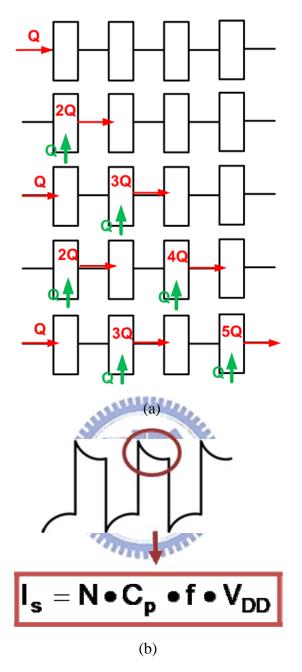


Fig. 4.8 (a) The steps of the charges are transferred during the clock period, and (b) it is the voltage waveform of a pumping node in a charge pump circuit.

4.3.3 Simulations for Different VDD

For the 2.5-V process, Fig. 4.9 shows the efficiency in different VDD. The efficiency of this work (the new proposed charge pump circuit) is upper than 80% in any supply voltage. The efficiency of the prior art circuit is lower than the efficiency of this work, but it has a little rising tendency because of the less leakage current produced in the low supply VDD. Fig.

4.10 shows the output ripples in different VDD, and the ripple is

$$Ripple(\%) = \frac{V_{pp}}{Vout} \bullet 100, \qquad (4.1)$$

where V_{pp} is the peak-to-peak value of Vout. Since this work can reduce the leakage current, the ripple of this work is smaller than the prior art circuit. For VDD=3V, the ripple of this work is 0.27% and the prior art circuit is 0.96%. For VDD=1V, the ripple of this work is 0.006% and the prior art circuit is 0.09%. If the ripple is small enough, the output is more suitable to connect with other circuit which needs the higher voltage (lower voltage). And in Fig. 4.11, for VDD=3V, the output voltage of this work is 14V and the prior art circuit is 13.3V. For VDD=1V, the output voltage of this work is 4.94V and the prior art circuit is 4.91V. Therefore, this work can operate in low supply voltage and apply in low-voltage process.

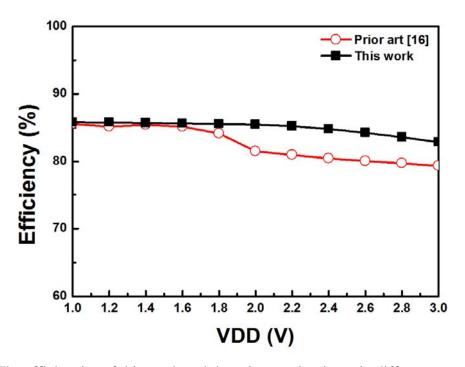


Fig. 4.9 The efficiencies of this work and the prior art circuit are in different supply voltages VDD with the $1\text{Meg}\Omega$ loading resistance.

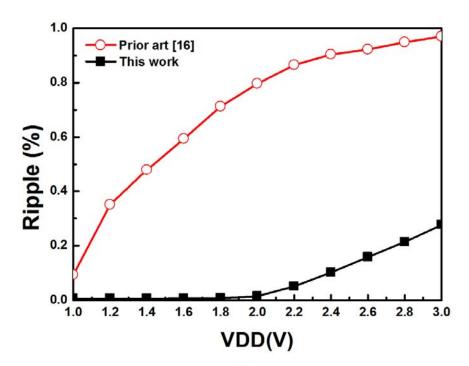


Fig. 4.10 The output ripples of this work and prior art circuit are in different supply voltages VDD and without loading resistance (Rout).

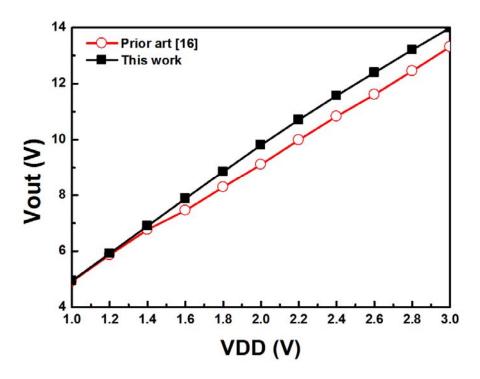


Fig. 4.11 The output voltage decreases when the supply voltages are decreasing and without loading resistance (Rout).

Chapter 5

Measured Results of the New Proposed Charge Pump Circuit

A test chip has been fabricated in a 65-nm CMOS process with 2.5-V device to verify the new proposed charge pump circuit and the prior-art circuit (Fig. 3.15). Each size of devices in these charge pump circuits is show in Table 5.1. The chip photograph, which contains Bulk (twin-well process) and DNW (deep n-well process), is shown in Fig. 5.1, the chip sizes are 350μm*415μm for the prior art and 385μm*440μm for the new proposed charge pump circuit.

Table 5.1 For the fair comparison, each size of all devices have to the same in different charge pump circuits.

THE PERSON NAMED IN

	Prior art [16]	This work
PMOS (μm/μm)	8/0.28	8/0.28
NMOS (µm/µm)	4/0.18	4/0.28
PMOS _{small} (μm/μm)	0	0.4/2
C _{pump} (pF)	2	2
C _{small} (fF)	0	25
C _{out} (pF)	20	20
CLK	2	4
VDD (V)	1.8	1.8
Frequency (MHz)	10	10
Stage number	4	4

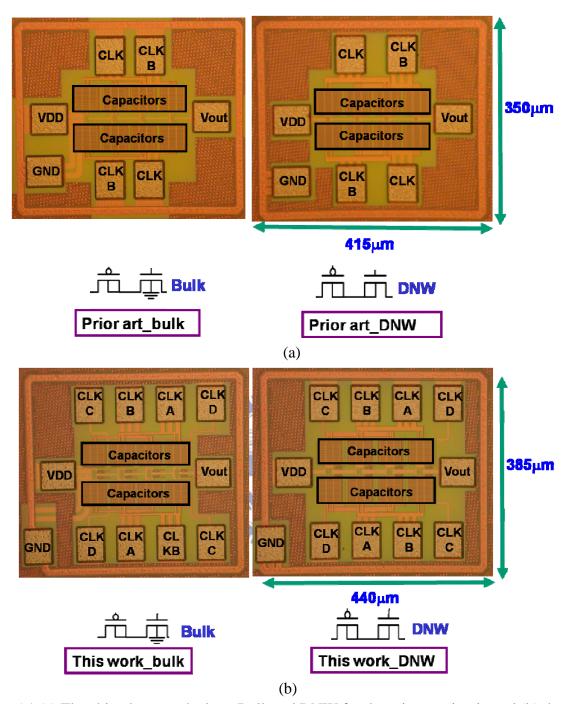


Fig. 5.1 (a) The chip photograph about Bulk and DNW for the prior art circuit, and (b) the new proposed charge pump circuit, fabricated in a 65-nm CMOS process.

5.1 THE PRIOR ART CIRCUIT [16]

The charge pump circuit of the prior art needs two clock signals, one input, and one output, so the measurement setup is shown in Fig. 5.2. The power supply is connected to the

input of the chip, clock generator is connected to the clock input of the chip, and the output of this chip is connected to the scope to observe the output waveforms in different resistors. The clock signals of this prior art is measured to shown in Fig, 5.3, with frequency is 10MHz, amplitudes are 1.8V, and the rise/fall time is 2ns. The measurement result is shown in Fig. 5.4. Additionally, the output voltage is 7.96V for the bulk process and 8V for the DNW process. Fig. 5.5 shows the measurement results of each chip of the prior art with the bulk process and DNW process. Finally, it shows the average measured outputs compared with the simulated results in Fig. 5.6. The output voltages without loading are 8.28V for simulation, 7.84V for the bulk process, and 7.98V for DNW process. For different supply voltage shown in Fig. 5.7, the highest supply voltage of the prior art circuit in bulk process is only at 1.8V, because the breakdown voltage of this prior art circuit is about 10V. From this measured result, the output voltage in DNW process is similar to the result of the simulation. Hence, the simulation result of the prior art circuit is 9.98V and the output voltage in DNW process is 9.88V for VDD=2.2V. The output voltage in the bulk process is 7.8V in the bulk process.

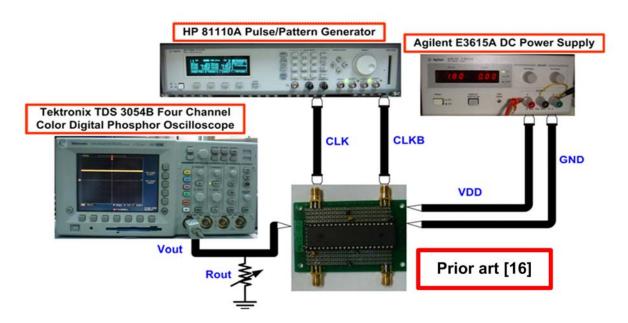


Fig. 5.2 The measurement setup of the prior art circuit.

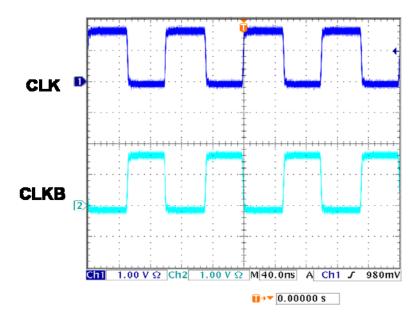


Fig. 5.3 The clock waveforms of the prior art circuit.

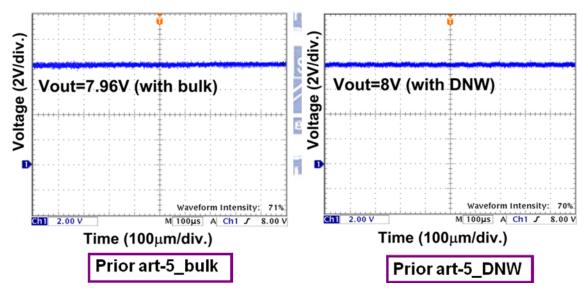


Fig. 5.4 The measured outputs of the prior art circuit.

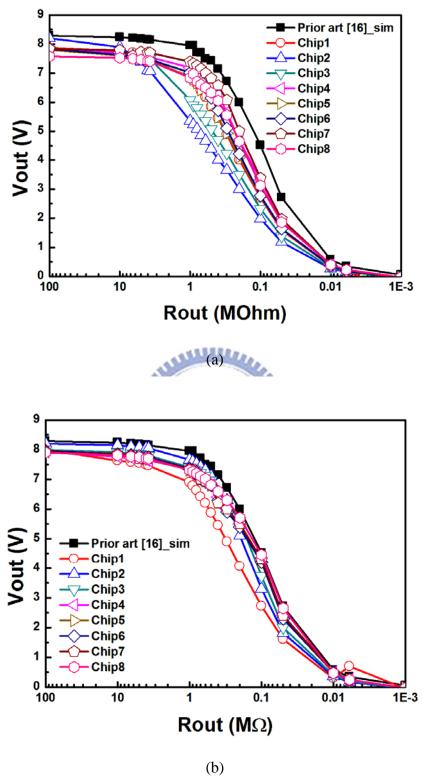


Fig. 5.5 The measurement results of each chip in (a) bulk process and (b) DNW process.

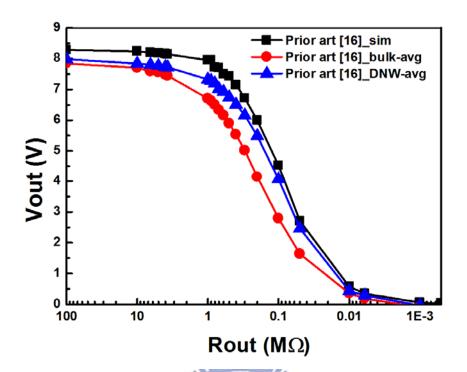


Fig. 5.6 The average output voltages about the prior art circuit with bulk process, DNW process, and simulation.

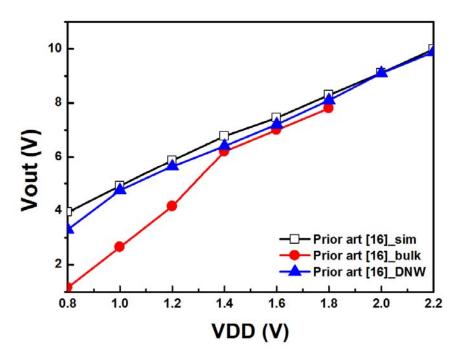


Fig. 5.7 The output voltages in different supply voltages VDD and without loading resistance (Rout).

5.2 THE NEW PROPOSED CHARGE PUMP CIRCUIT (THIS WORK)

This work needs four clock signals, one input, and one output, so the measurement setup is shown in Fig. 5.8 The power supply is connected to the input of the chip, clock generator is connected to the clock input of the chip, and the output of this chip is connected to the scope to observe the output waveforms in different resistors. This work needs four-phase clock, so it needs two 81110A clock generators to provide clock signal. Therefore, it has to add another function generator to connect with two 81110A for the reason of the synchronization.

The clock signals of this work are measured to shown in Fig. 5.9, with frequency is 10MHz, amplitudes are 1.8V, and the rise/fall time is 2ns. In Fig. 5.9 (b), each clock signals are non-overlapping, and the time of T_2 and T_4 are 2ns to let all devices in this work cut off. The measured results of output voltages are shown in Fig. 5.10. Additionally, the output voltage is 8.68V for the bulk process and 8.8V for the DNW process. Fig. 5.11 shows the measured results of each chip of this work with the bulk process and DNW process. And finally, it shows the average measured output compared with the simulated results in Fig. 5.12. The output voltages without loading are 8.85V for simulation, 8.68V for the bulk process, and 8.83V for DNW process. For different supply voltage shown in Fig. 5.13, the highest supply voltage of the prior art circuit in bulk process is only at 1.8V, because the breakdown voltage of this prior art circuit is about 10V. From this measured result, the output voltage in DNW process is similar to the result of the simulation. Hence, the simulation result of the prior art circuit is 10.7V and the output voltage in DNW process is 10.3V for VDD=2.2V. The output voltage in the bulk process is 8.7V in the bulk process.

The comparison is shown in Fig. 5.14, and it is apparent that the output voltage of this work is better than the prior art no matter what in the bulk process or in DNW process. Fig. 5.15 shows the output voltages in different supply voltages, and this work is compared with

the prior art circuit. From this result, the measured results of this work is better than the prior art circuit.

If the process drifts, the rise/fall time will increase due to the process or the layout lines. Hence, on the situation of the clock errors, the output voltage would be decreased when the rise/fall time of the clocks increases. Fig. 5.16 shows the measurement results in different rise/fall times to verify the simulation result in Fig. 4.7.

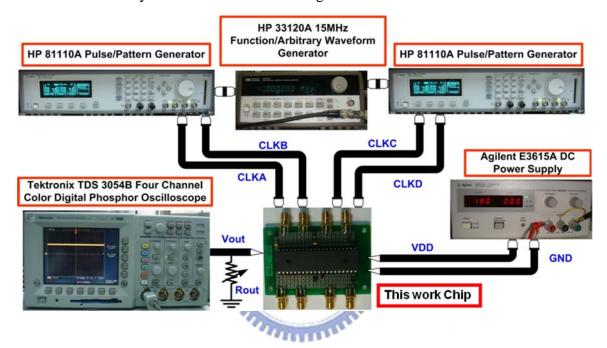
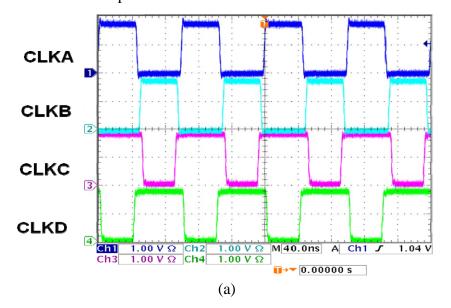


Fig. 5.8 The measurement setup of this work.



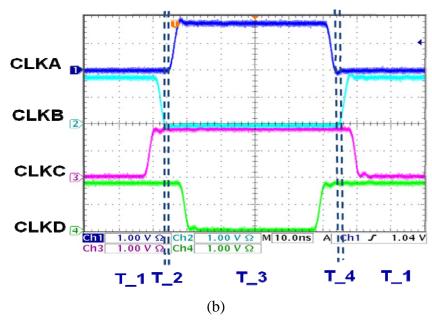


Fig. 5.9 (a) The clock waveforms of this work, and (b) the time intervals in a clock period with 2ns of T_2 and T_4 time.

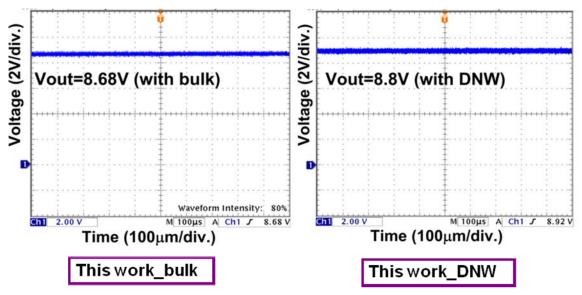


Fig. 5.10 The measured outputs of this work.

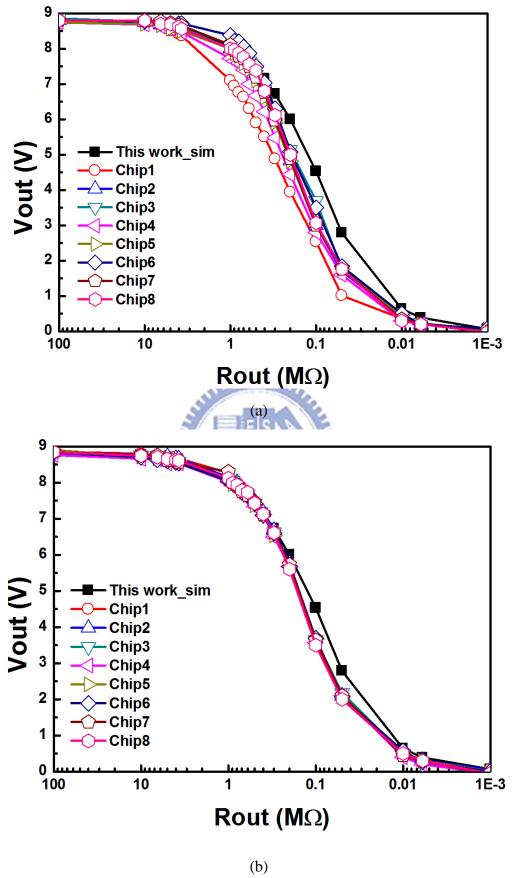


Fig. 5.11 The measured results of each chip in (a) the bulk process and (b) DNW process.

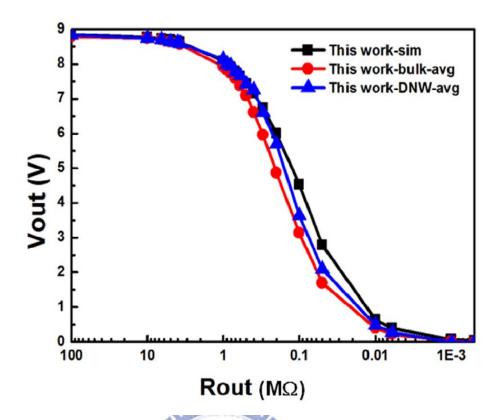


Fig. 5.12 The average output voltages about this work with bulk process, DNW process, and simulation.

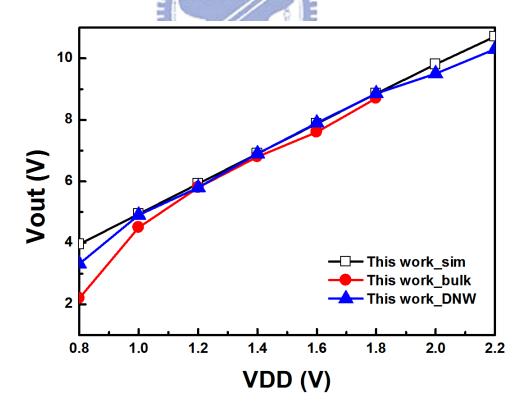


Fig. 5.13 The output voltage in different supply voltages VDD and without loading resistance (Rout).

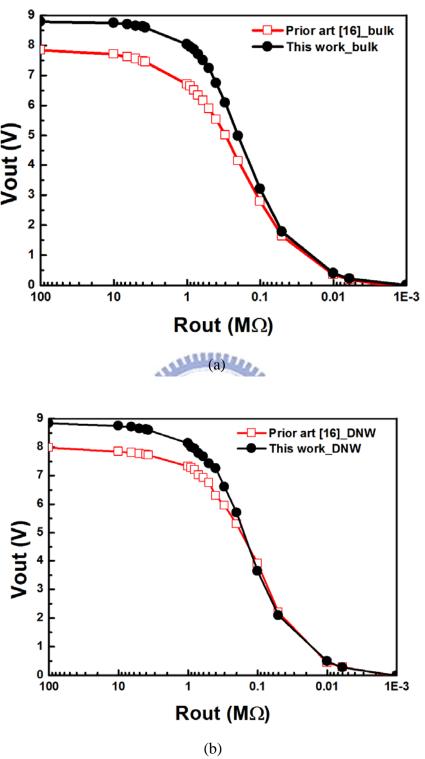


Fig. 5.7 The comparison of this work and the prior art circuit in the (a) bulk process and (b) DNW process (f=10MHz, VDD=1.8V, rise/fall time of ~2ns), with different loading resistance (Rout) at the output node.

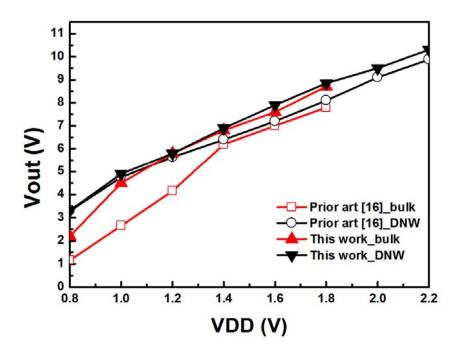


Fig. 5.15 The comparison of the prior art circuit and this work in different supply voltages VDD and without loading resistance (Rout).

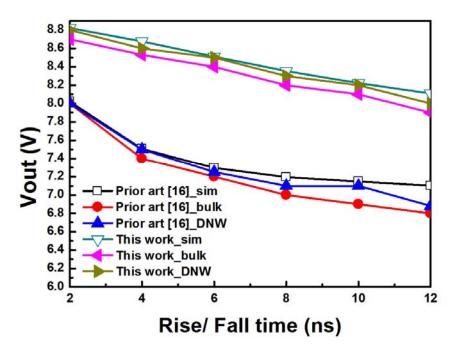


Fig. 5.16 The variations of the output voltage in different rise/fall times of the clocks and without loading resistance (Rout).

Chapter 6

Conclusions and Future Works

6.1 CONCLUSIONS

By inserting a short turn-off period into the circuit operation of charge pump circuit, the return-back leakage current during the clock transition can be successfully suppressed in the new proposed charge pump circuit realized in 65-nm COMS process. Therefore, the new proposed charge pump circuit has better efficiency than that of the prior designs, and also without suffering the gate oxide reliability issue in a low-voltage CMOS process. Besides, the new proposed charge pump circuit also has a better performance if the clock signals are not ideal in the long rise/fall time. And from the simulation, the new proposed charge pump circuit has good efficiency to be utilized in the low-power system suitably. Finally, the proposed charge pump circuit is very suitable for applications in low-voltage CMOS integrated circuits to efficiently generate the higher voltage.

6.2 FUTURE WORKS

In the memory systems, the stable high voltage (or negative voltage) is needed to program or erase data in the memory cells, so the feedback loop of the charge pump circuit should be further developed in the future [18], shown in Fig. 6.1.

The on-chip four-phase clock generator should be integrated in the new proposed charge pump circuit.

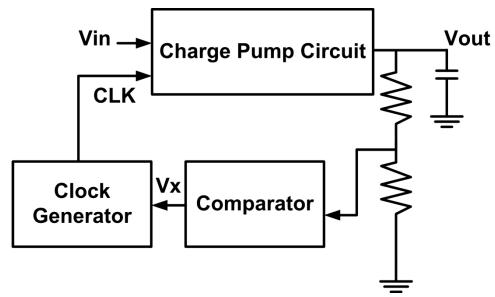


Fig. 6.1 The feedback loop of the charge pump circuit.



REFERENCES

- [1] J. D. Cockcroft and E. T. S. Walton, "Production of high velocity positive ions," *Proceedings of the Royal Society, Series A*, Vol.136, pp. 619-630, 1932.
- [2] J. F. Dickson, "On chip high-voltage generation in MNOS integrated circuits using an improved voltage multiplied technique," *IEEE J. Solid-State Circuits*, vol. 1, pp. 374-378, Jun. 1976.
- [3] T. Jinbo, H. Nakata, K. Hashimito, T. Watanabe, K. Ninomiya, T. Urai, M. Koike, T. Sato, N. Kodama, K. Oyama, and T. Okazawa, "A 5-V-only 16-Mb flash memory with sector erase mode," *IEEE J. Solid-State Circuits*, vol. 27, pp. 1547-1554, Nov. 1992.
- [4] S. Atsumi, M. Kuriyama, A. Umezawa, H. Banba, K. Naruke, S. Yamada, Y. Ohshima, M. Oshikiri, Y. Hiura, T. Yamane, and K. Yoshikawa, "A 16-Mb flash EEPROM with a new self-data-refresh scheme for a sector erase operation," *IEEE J. Solid-State Circuits*, vol. 29, pp. 461-469, Apr. 1994.
- [5] C. Yoo and K.-L. Lee, "A low-ripple poly-si TFT charge pump for driver-integrated LCD panel," *IEEE Trans. Consumer Electronics*, vol. 51, No. 2, pp. 606-610, May 2005.
- [6] J. S. Witters, G. Groeseneken, and H. E. Maes, "Analysis and modeling of on-chip high-voltage generator circuits for use in EEPROM circuits," *IEEE J. Solid-State Circuits*, vol. 24, pp. 1372-1380, Oct. 1989.
- [7] K. Sawada, Y. Sugawara, and S. Masui, "An on-chip high-voltage generator circuit for EEPROM with a power supply voltage below 2V," in *Symp. VLSI Circuits Dig. Tech. Papers*, 1992, pp. 75–76.
- [8] K.-H. Choi, J.-M. Park, J.-K. Kim, T.-S. Jung, and K.-D. Suh, "Floating-well charge pump circuits for sub-2.0 V single power supply flash memories," in *Symp. VLSI Circuits Dig. Tech. Papers*, 1997, pp. 61-62.
- [9] J.-T. Wu and K.-L. Chang, "MOS charge pump for low-voltage operation," *IEEE J. Solid-State Circuits*, vol. 33, pp. 592–597, Apr. 1998.
- [10] H. Lin, K.-H. Chang, and S.-C. Wong, "Novel high positive and negative pumping circuits for low supply voltage," in *Proc. IEEE Int. Symp. Circuits Syst.*, 1999, vol. I, pp. 238–241.
- [11] S.-Y. Lai and J.-S. Wang, "A high-efficiency CMOS charge pump circuit," in *Proc. IEEE Int. Symp. Circuits Syst.*, 2001, vol. IV, pp.406–409.

- [12] J. Shin, I.-Y. Chung, Y. J. Park, and H. S. Min, "A new charge pump without degradation in threshold voltage due to body effect," *IEEE J. Solid-State Circuits*, vol. 35, pp. 1227–1230, Apr. 2000.
- [13] H. Lin and N.-H. Chen, "New four-phase generation circuits for low voltage charge pumps," in *Proc. IEEE Int. Symp. Circuits Syst.*, 2001, vol. I, pp. 504–507.
- [14] E. Racape and J. M. Dage, "A PMOS-switch based charge pump, allowing lost cost implementation on a CMOS standard process," in *Proc. ESSCIRC*, pp. 77-80, Sept. 2005.
- [15] J. Pan and T. Yoshihara, "A charge pump circuit without overstress in low-voltage CMOS standard process," in *Proc. IEEE Conf. on Electron Device and Solid-State Circuits*, 2007, pp. 501-504.
- [16] M.-D. Ker, S.-L. Chen, and C.-S. Tsai, "Design of charge pump circuit with consideration of gate oxide reliability in low-voltage CMOS process," *IEEE J. Solid-State Circuits*, vol. 41, pp. 1100–1107, May 2006.
- [17] G. Palumbo, D. Pappalardo, and M. Gaibotti, "Charge pump circuits: power-consumption optimization," *IEEE Trans. on Circuits and Systems I: Fundamental Theory and Applications*, vol.49, pp. 1535-1542, Nov. 2002.
- [18] T. Tanzawa, A. Umezawa, M. Kuriyama, T. Taura, H. Banba, T. Miyaba, H. Shiga, Y. Takano, and S. Atsumi, "Wordline voltage generating system for low-power low-voltage flash memories," *IEEE J. Solid-State Circuits*, vol. 36, pp.55-62, Jan. 2001.

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- [2] M.-D. Ker and <u>Yi-Hsin Weng</u> "Charge Pump Design in Low-Voltage CMOS Technology," US patent pending.

